

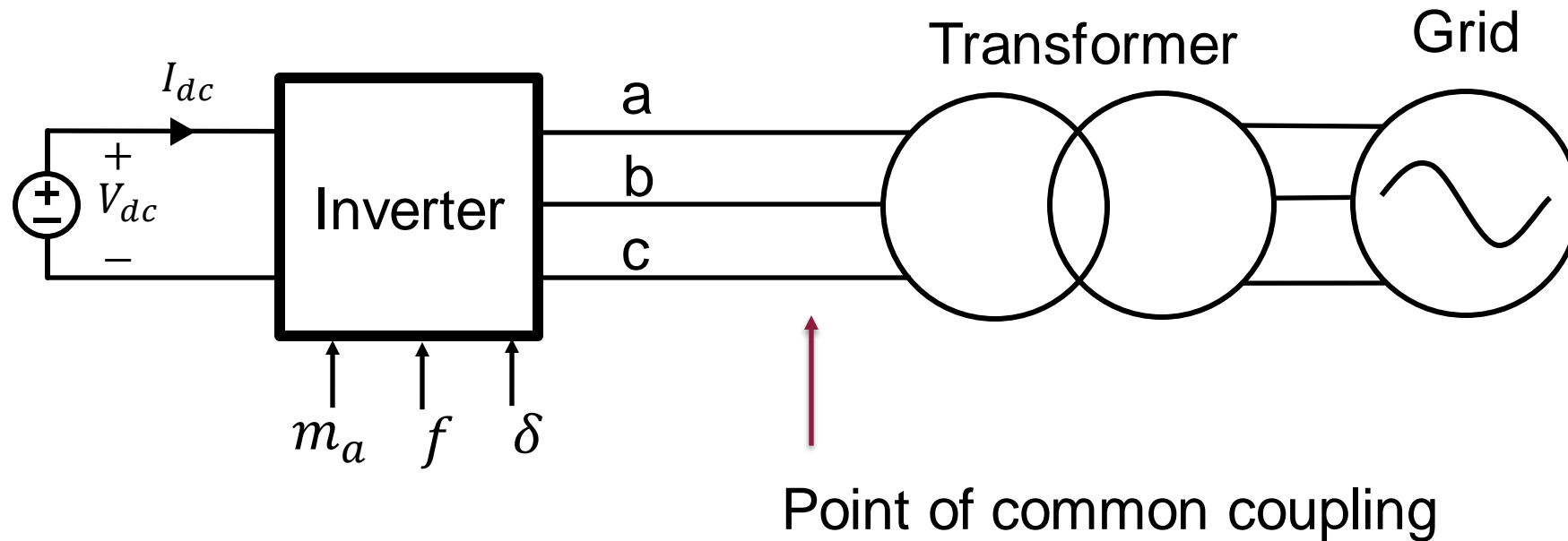
Module 3

Grid-Following Inverters

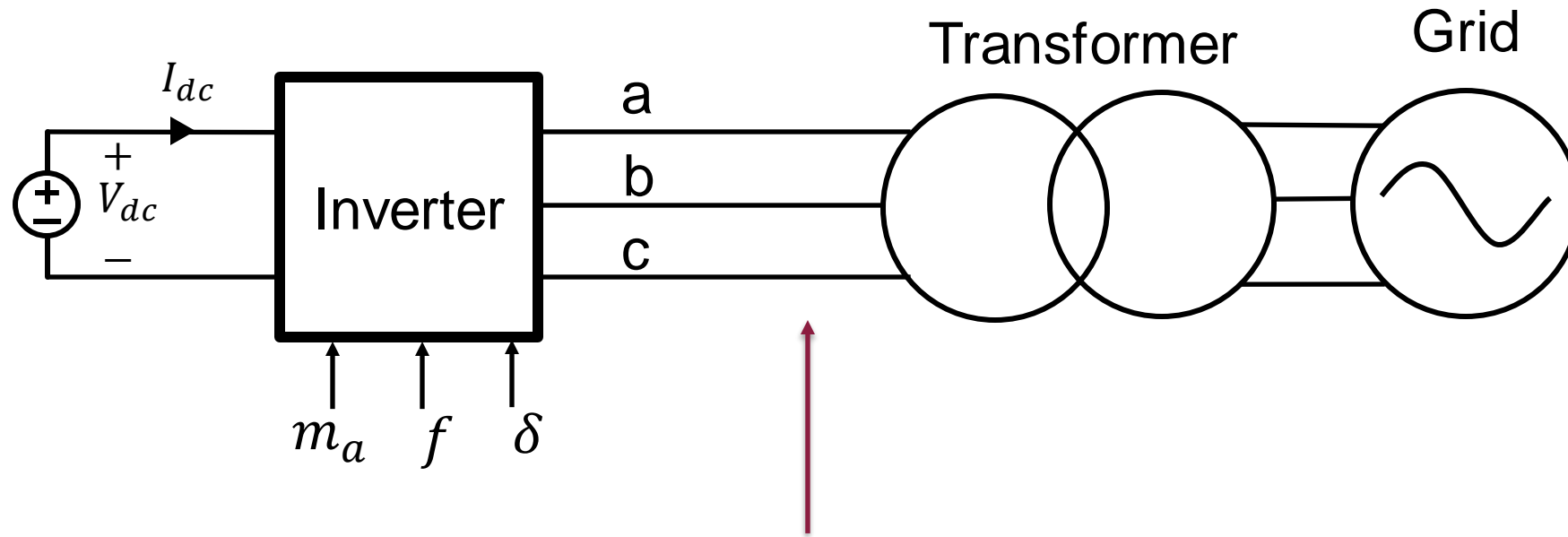
How do they work and what are they expected to do?

Key Assumption: The Stiff Grid

- Philosophy: “The grid exists, how do we connect to it?”

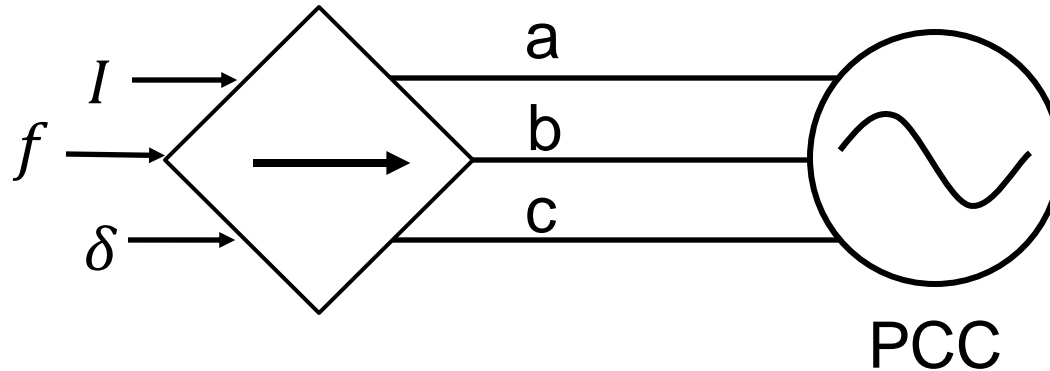


Key Assumption: The Stiff Grid



- Constant voltage magnitude
- Constant frequency
- Balanced
- Not only do we not provide inertia, we *rely* on inertia

Create a Controlled Current Source



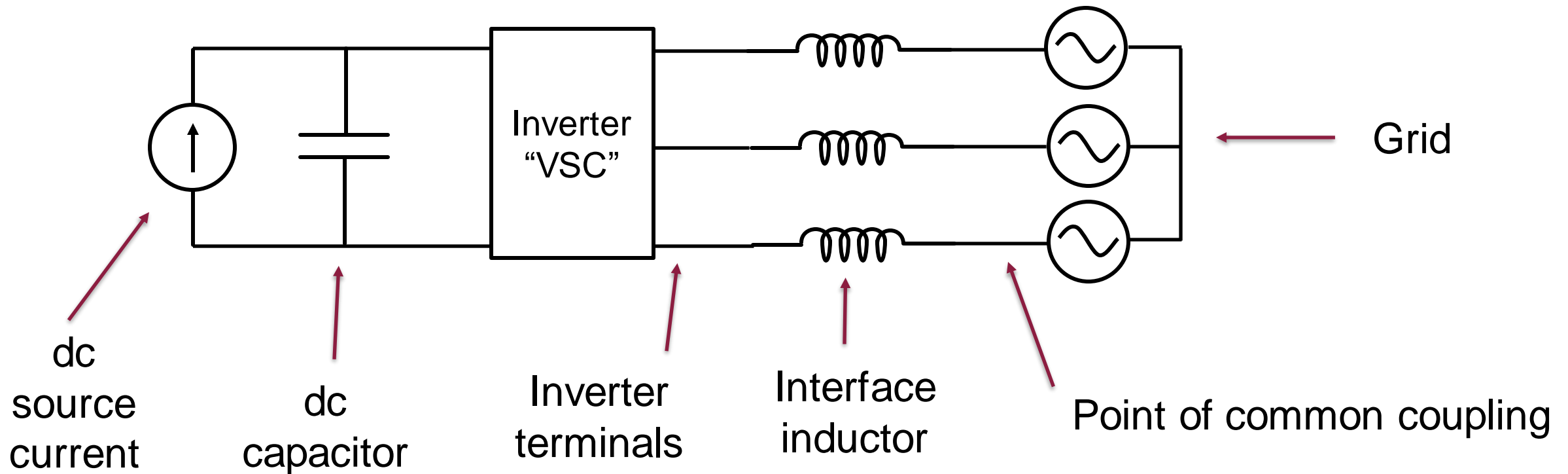
- Commanding magnitude and phase gives us power control
- Frequency must be equal to PCC

Reminder: Sinusoidal Power Transfer

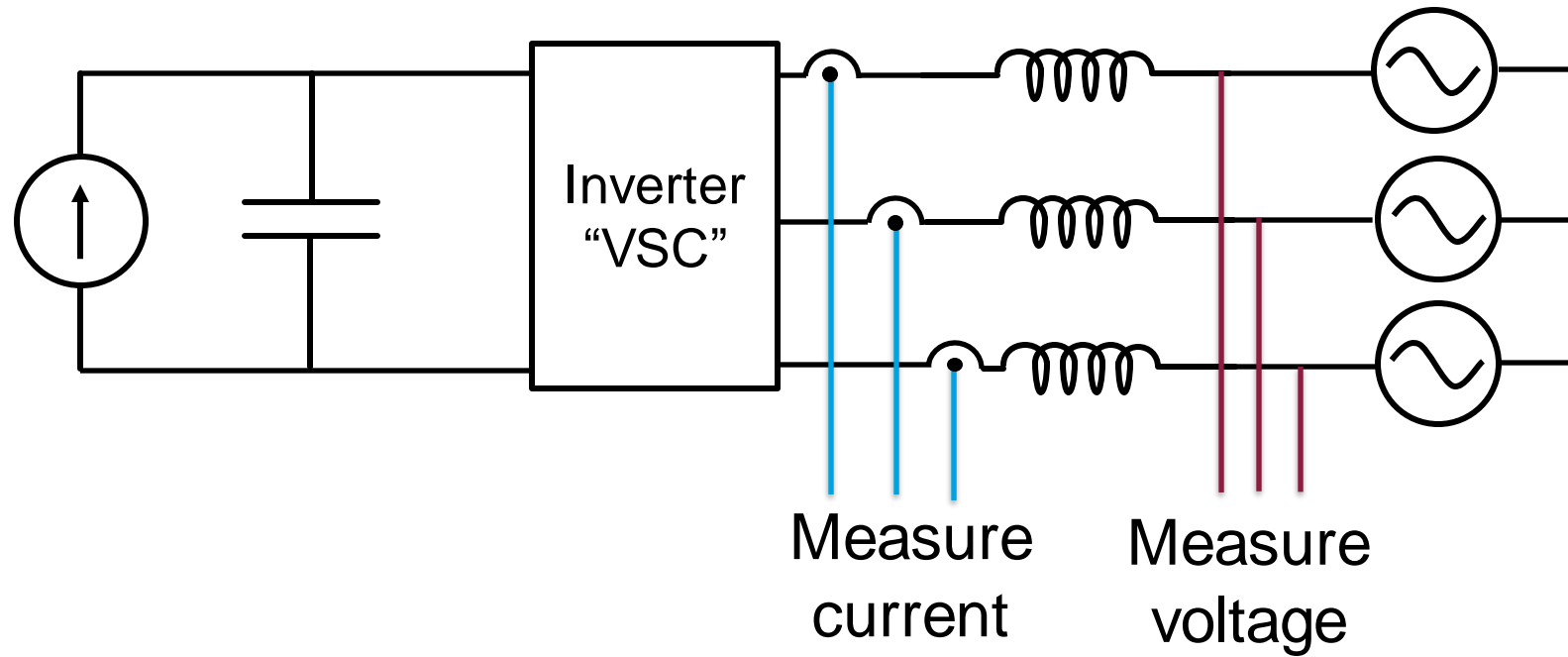
- The only way to transfer between sources is for them to have the same frequency
- $v(t) = V \sin(\omega_1 t)$
- $i(t) = I \sin(\omega_2 t)$
- $p(t) = VI \sin(\omega_1 t) \sin(\omega_2 t)$
- $p(t) = \frac{VI}{2} [\cos((\omega_1 - \omega_2)t) - \cos((\omega_1 + \omega_2)t)]$
- Average = 0 unless $\omega_1 = \omega_2$

Voltage-Sourced Converter System

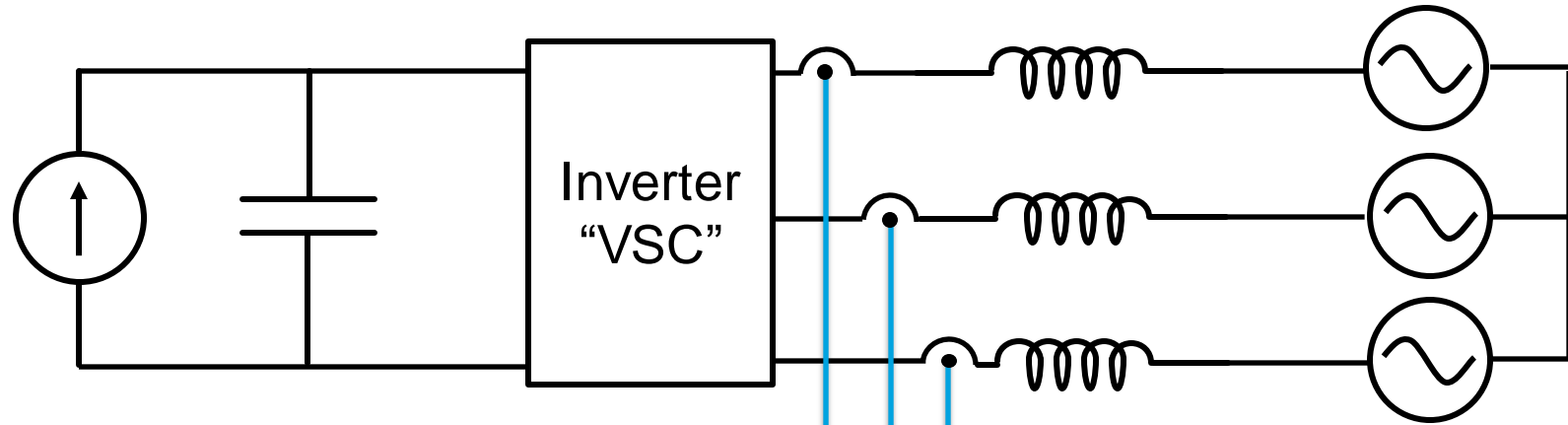
- The inverter system in practice is as follows



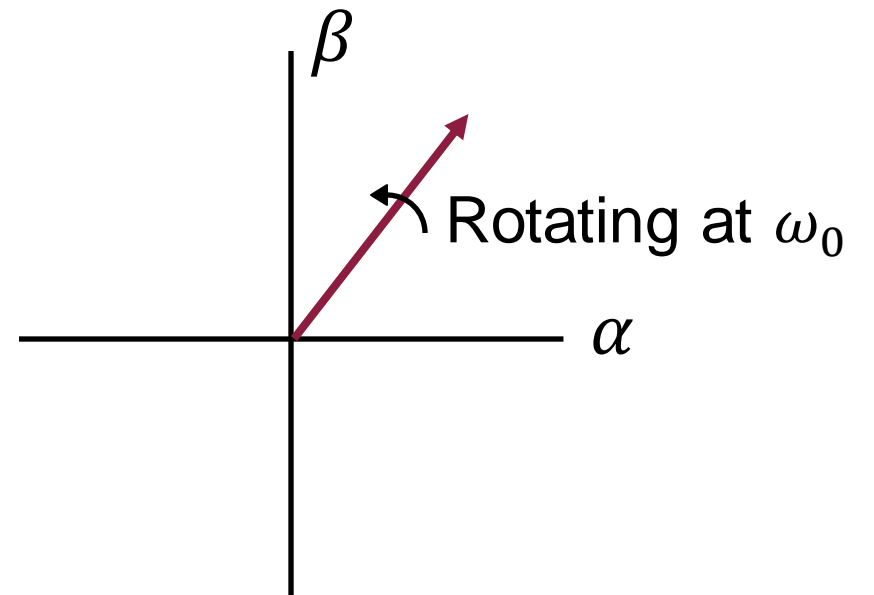
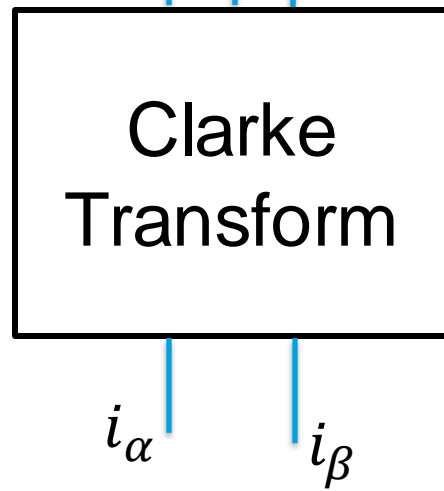
Voltage-Controlled Current Source



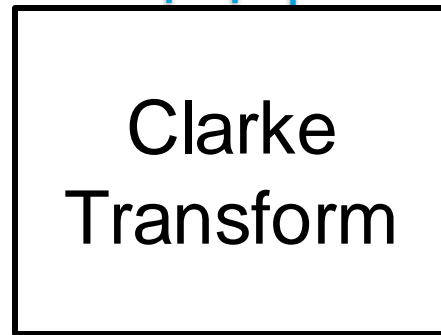
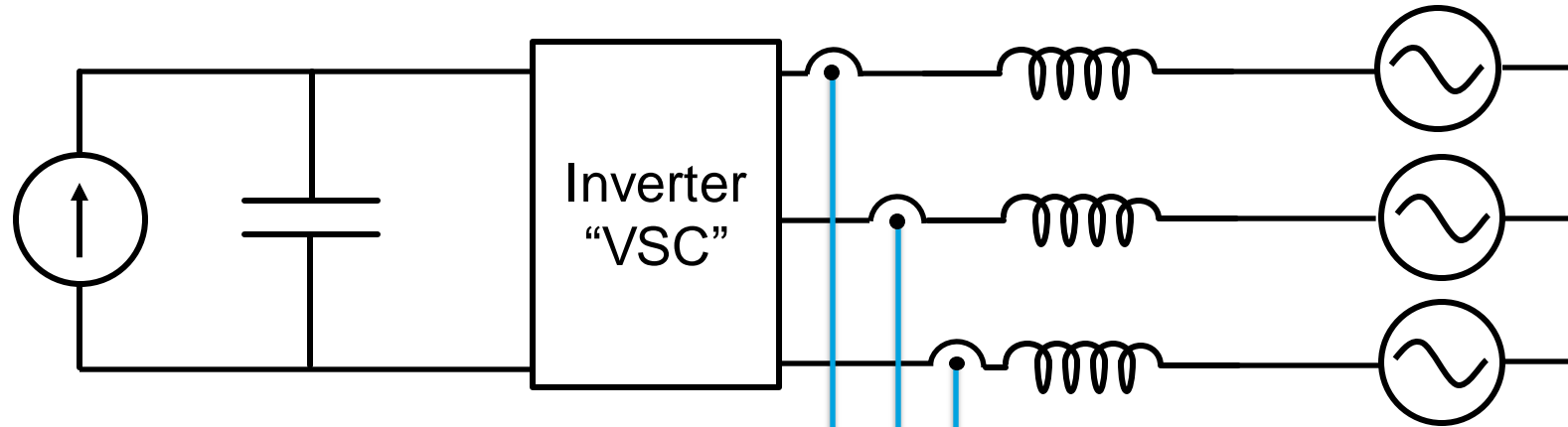
Alpha-beta Frame via Clarke Transform



$$C = \frac{2}{3} \begin{bmatrix} 1 & -\frac{1}{2} & -\frac{1}{2} \\ 0 & \frac{\sqrt{3}}{2} & -\frac{\sqrt{3}}{2} \\ \frac{1}{\sqrt{2}} & \frac{1}{\sqrt{2}} & \frac{1}{\sqrt{2}} \end{bmatrix}$$



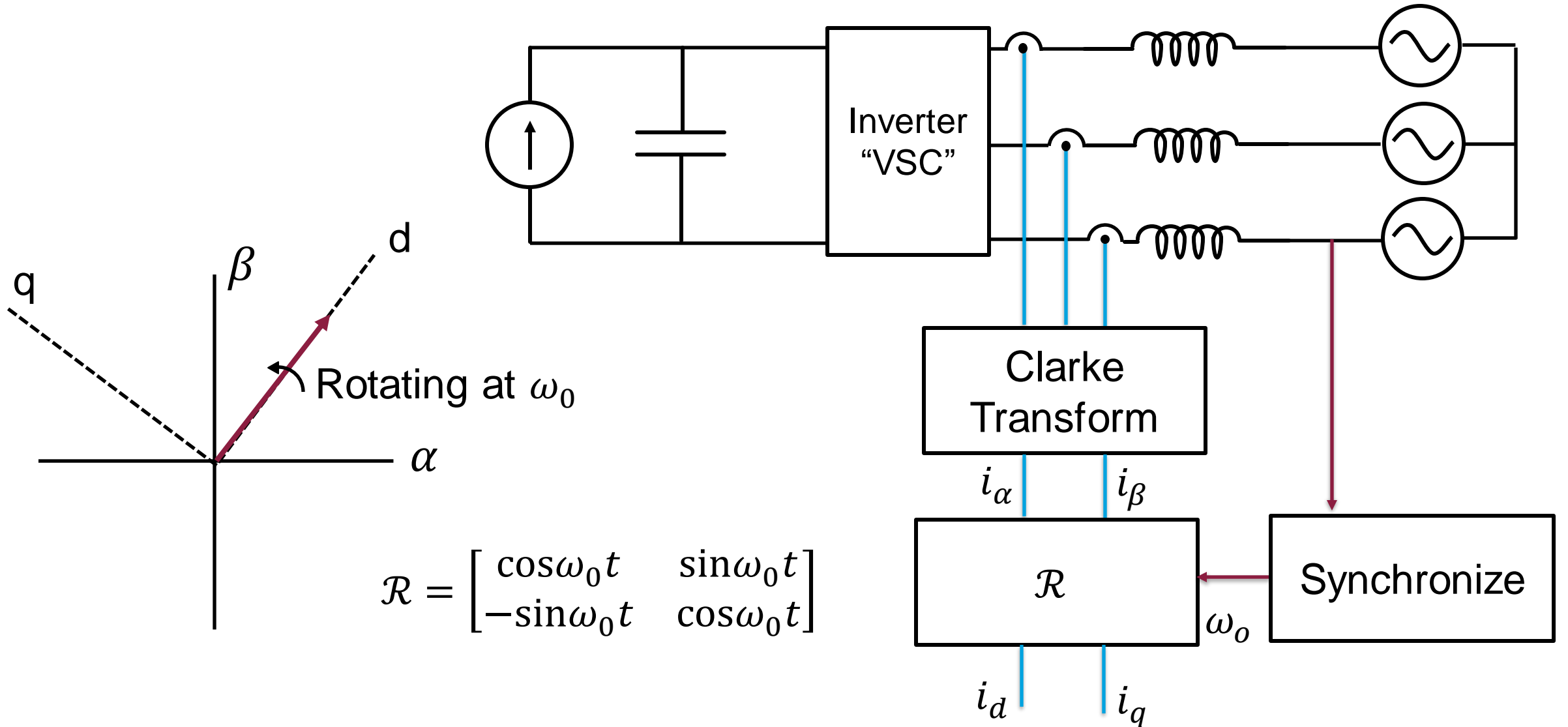
Alpha-beta Frame via Clarke Transform



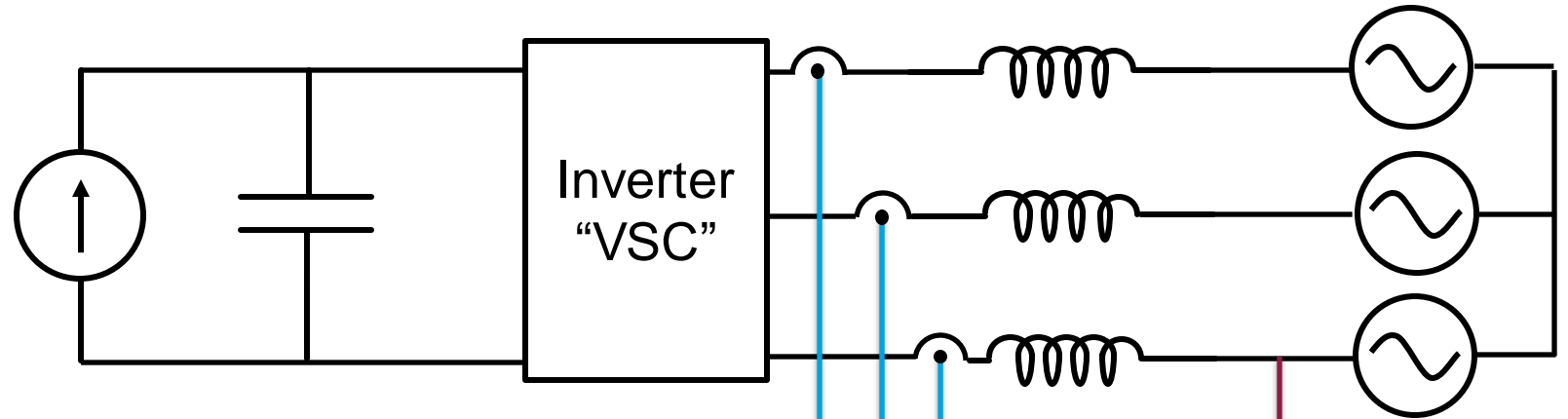
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- Reduce to two parameters
- Instantaneous measurements:
 - $p(t) = \frac{3}{2} (v_\alpha i_\alpha + v_\beta i_\beta)$
 - $q(t) = \frac{3}{2} (v_\beta i_\alpha - v_\alpha i_\beta)$

Stationary “dq” Reference Frame



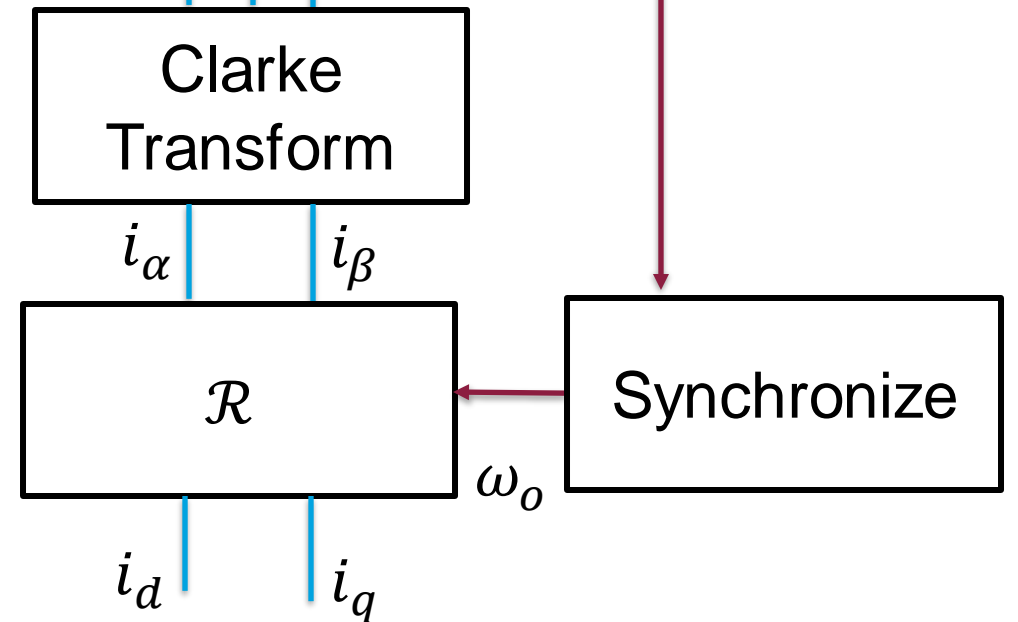
Stationary “dq” Reference Frame



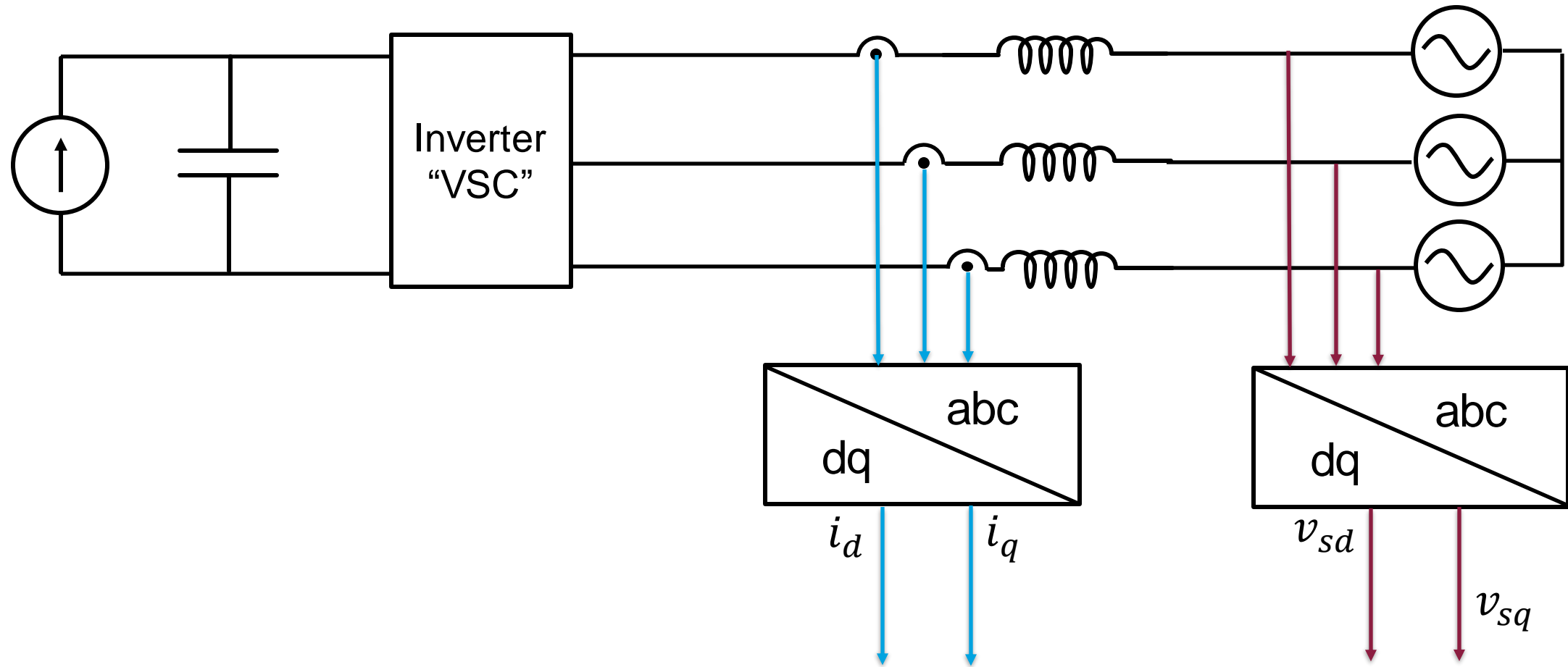
- Two **stationary (dc)** parameters
- Instantaneous measurements:

- $p(t) = \frac{3}{2} (v_d i_d + v_q i_q)$
- $q(t) = \frac{3}{2} (v_q i_d - v_d i_q)$

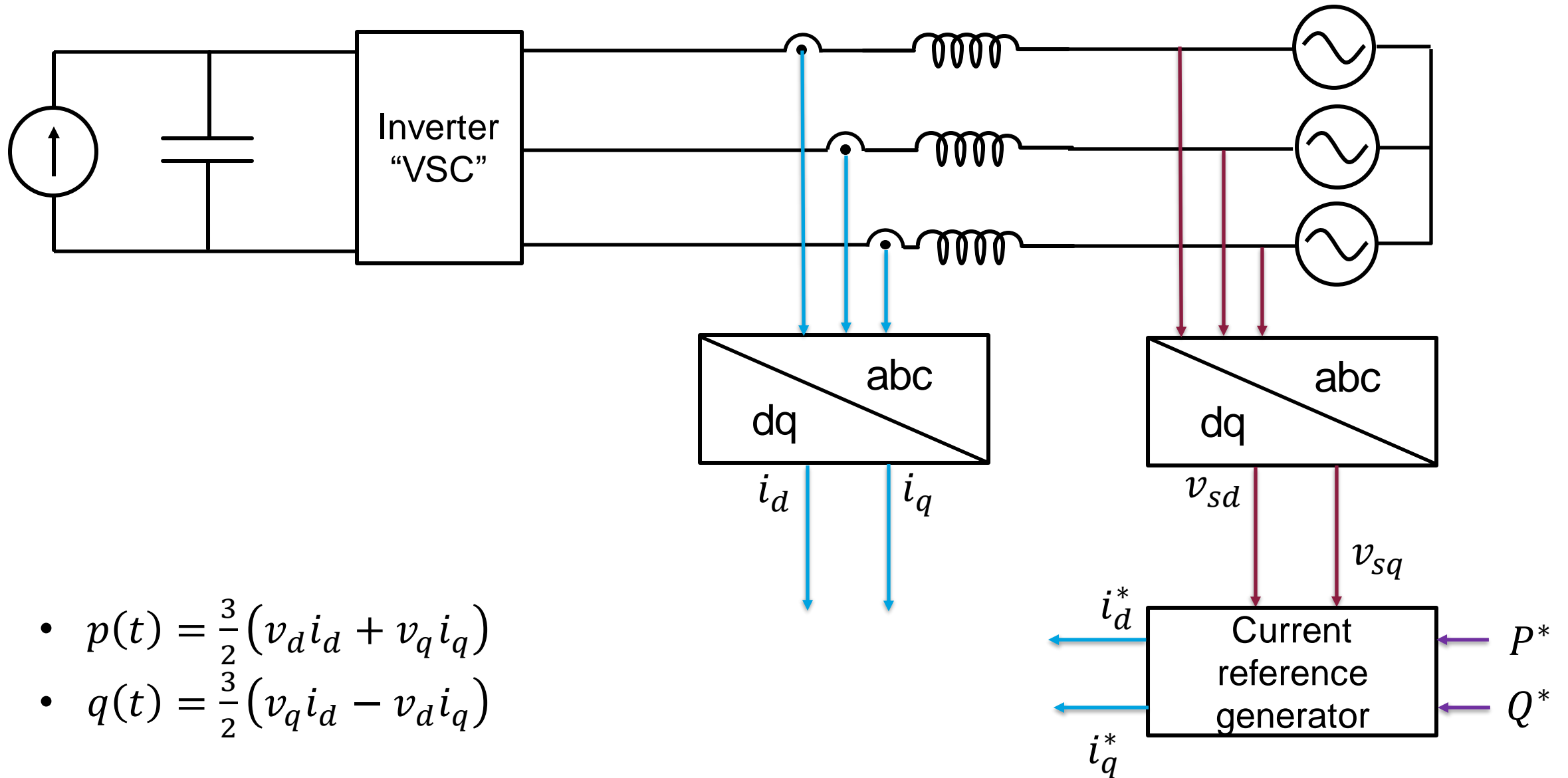
$$\mathcal{R} = \begin{bmatrix} \cos\omega_0 t & \sin\omega_0 t \\ -\sin\omega_0 t & \cos\omega_0 t \end{bmatrix}$$



Voltage-controlled Current Source

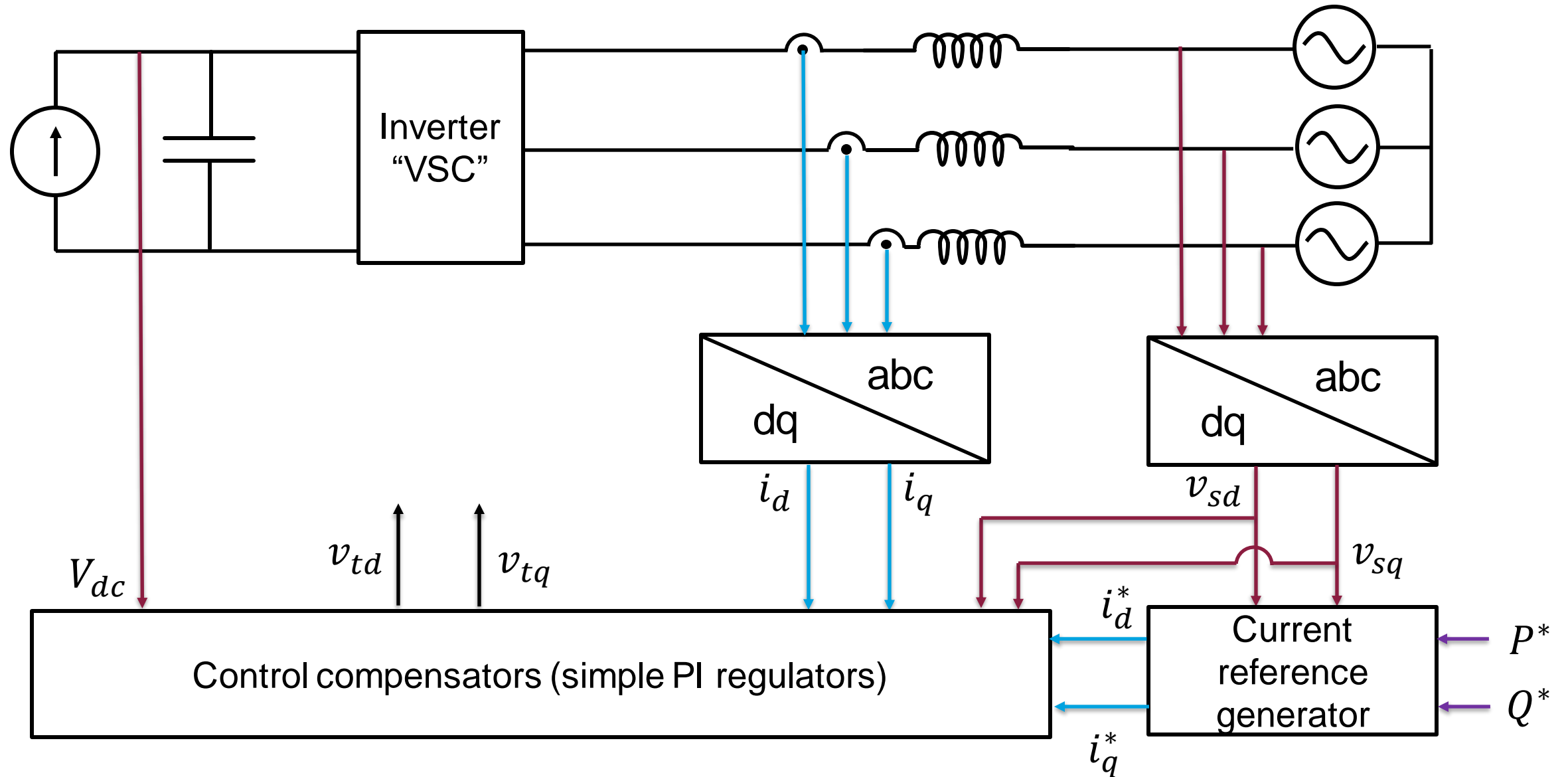


Voltage-controlled Current Source

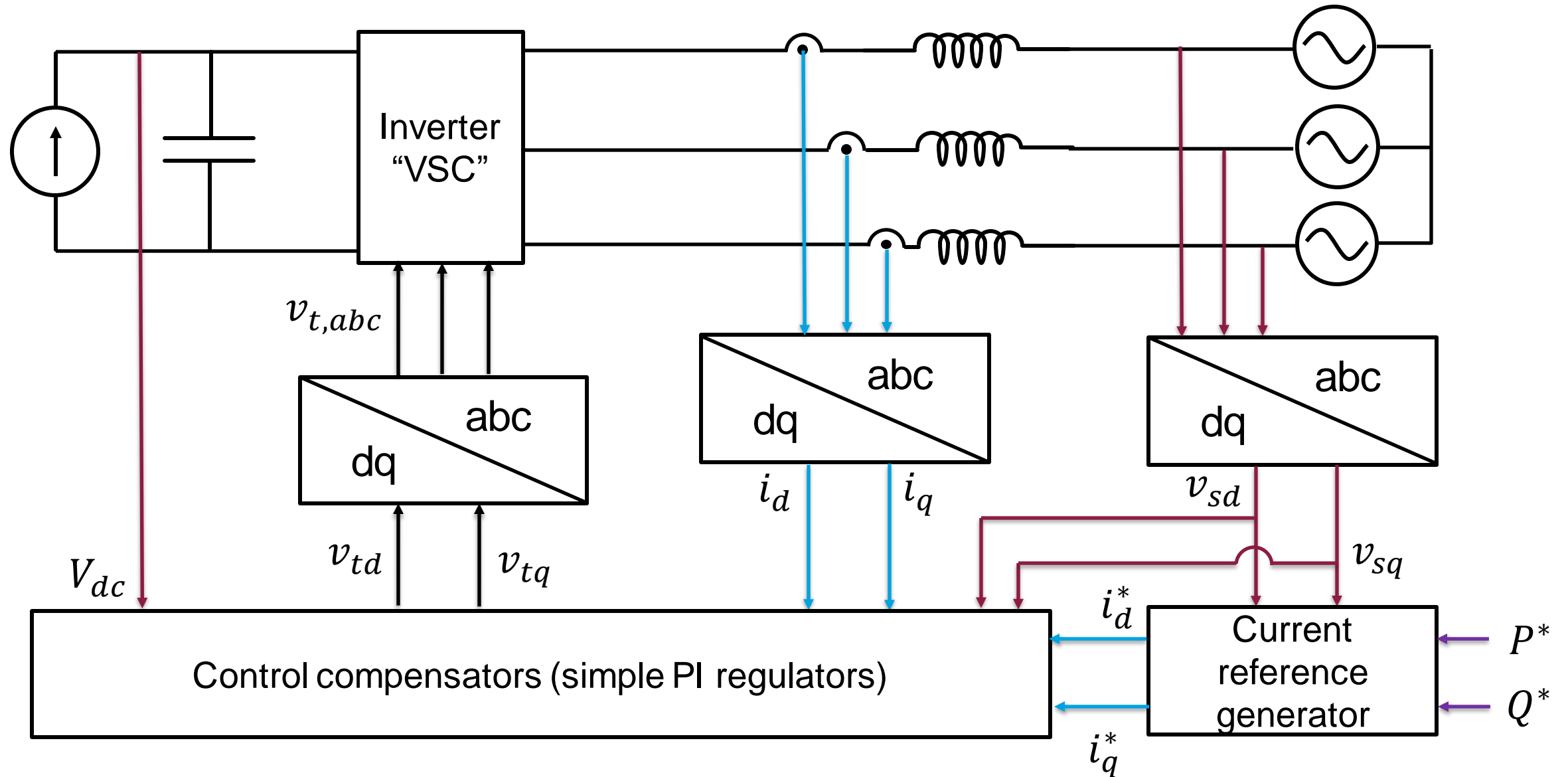


- $p(t) = \frac{3}{2} (v_d i_d + v_q i_q)$
- $q(t) = \frac{3}{2} (v_q i_d - v_d i_q)$

Voltage-controlled Current Source

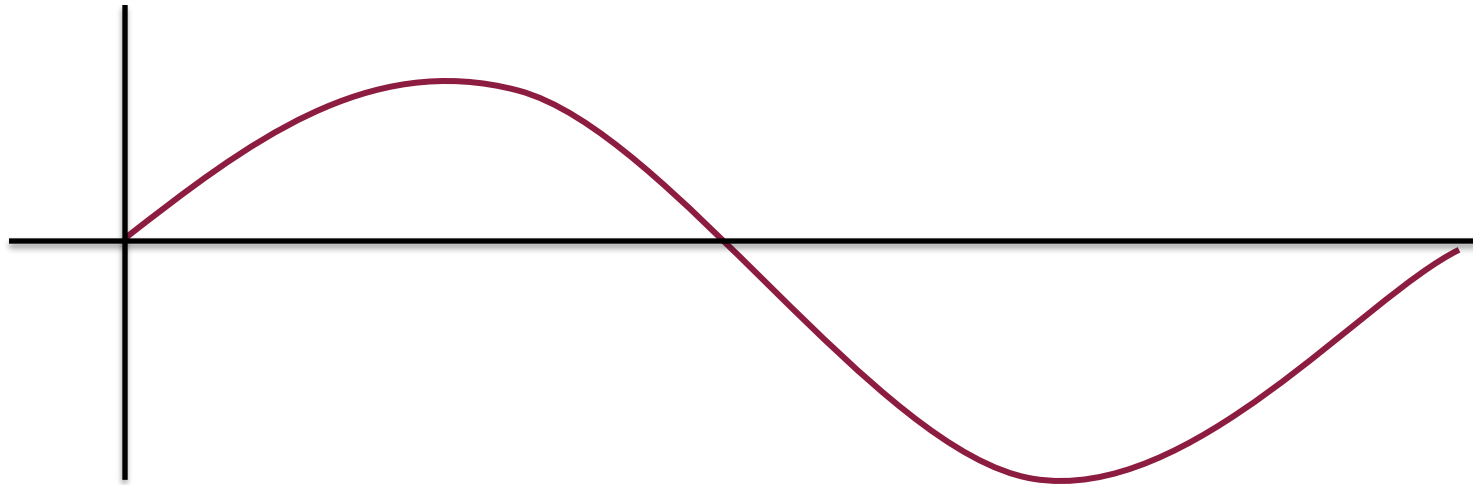


Voltage-controlled Current Source



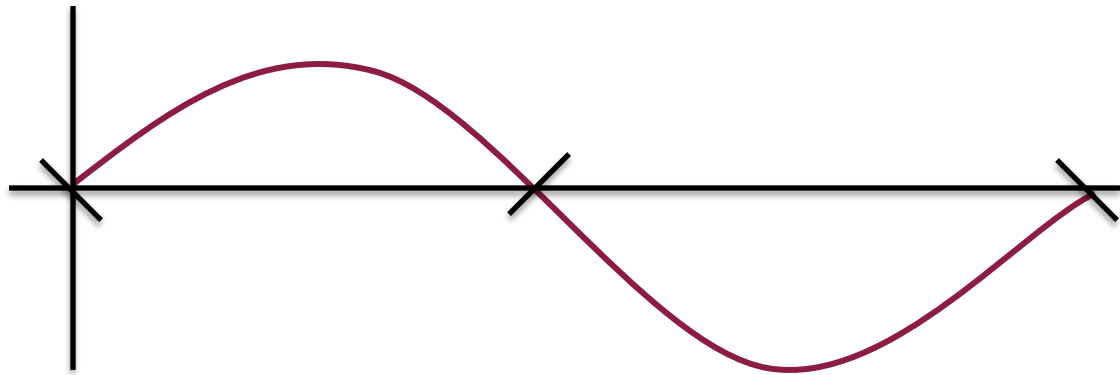
Important Detail: Synchronization

- If you have some sampled voltage $v(t)$, how do you track magnitude, frequency, and phase?
 - Magnitude: retain max value
 - Phase more complicated



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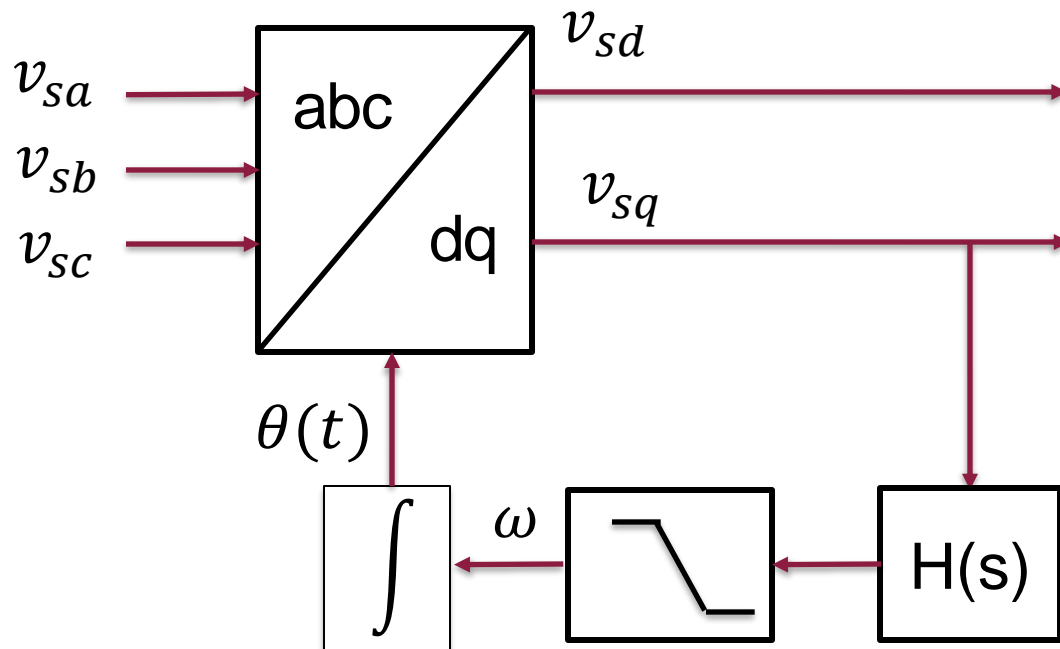


Crudely:

- zero-crossing detection
- Correlate sample time with sinusoidal LUT at assumed frequency

Synchronization: Phase-Locked Loop

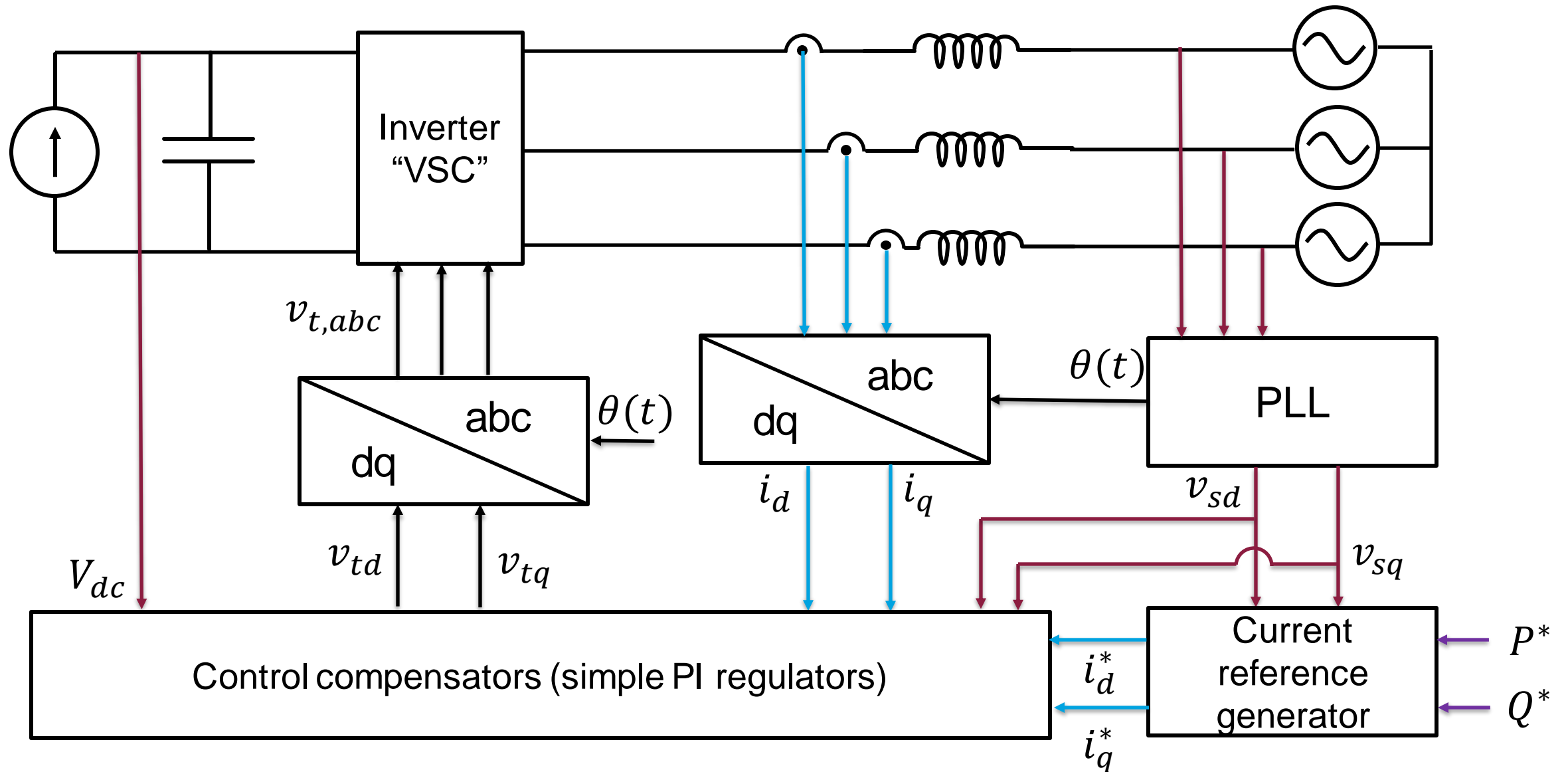
- Most popular, robust
- $\sin(\omega t + \phi) = \sin(\theta(t))$
 - Pull out $\theta(t)$ then we have what we need



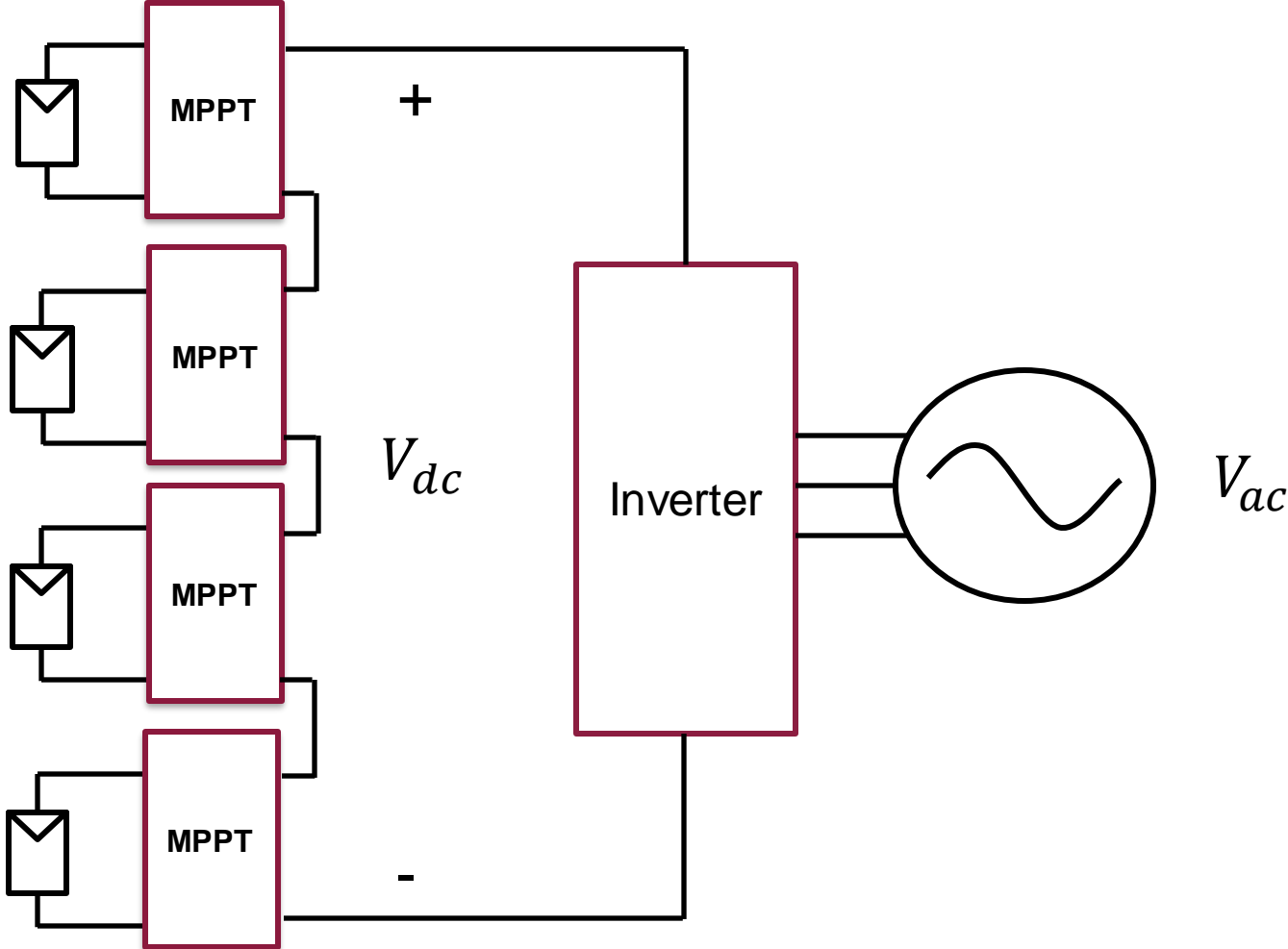
By definition, regulate v_{sq} to zero means synchronized to grid

Saturation – inherent assumption on min and max frequency

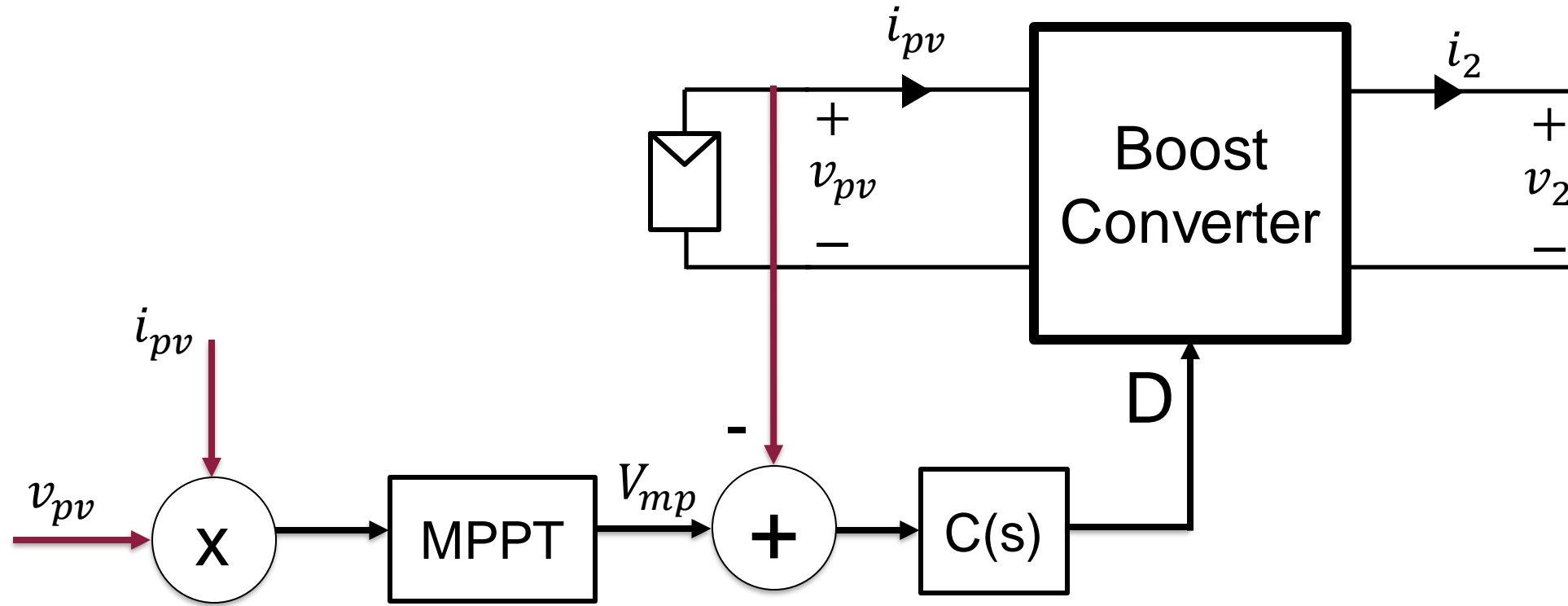
Voltage-controlled Current Source



Typical Solar PV Architecture

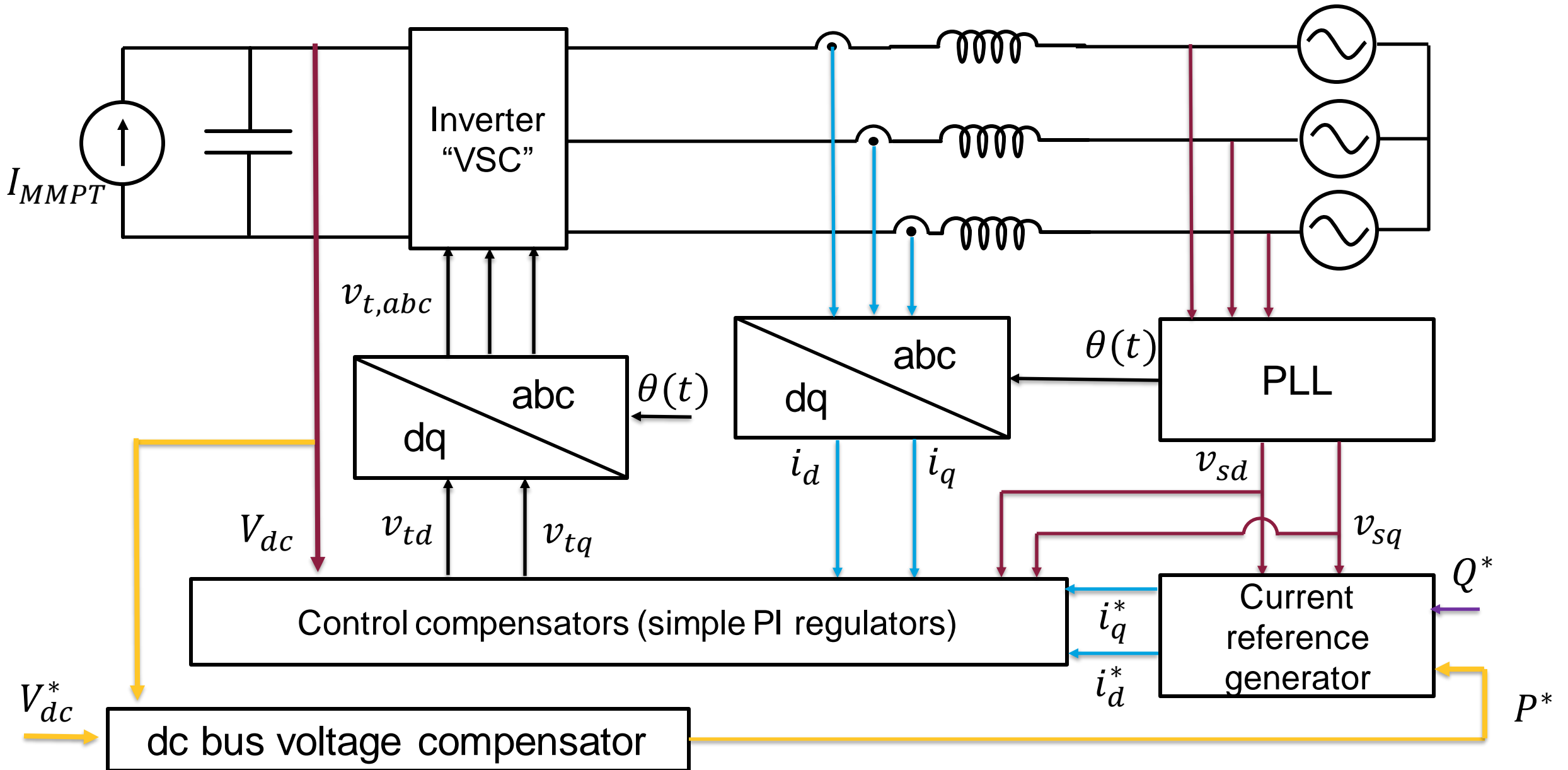


MPPT Tracker



Control D to extract maximum power

Inverter Regulates dc Bus



Operation During Atypical Conditions

- Previously, if V , f out of nominal conditions, disconnect!
- Today: regulations are being introduced which demand grid-support
 - “Ride-through” or “Grid supporting” capability
- Disadvantageous for revenue, since only rewarded for P generation.

Conclusions

- Grid-following inverters assume nominal voltage and frequency at point of common coupling
- System is “stiff” \Rightarrow Converter cannot change grid voltage
- Grid-following control synchronizes to the grid, typically with PLL