# Cyber-physical Interactions and Power Grid Reliability

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> PSERC Webinar November 22, 2016



# Introduction

- Modern power systems: integration of current carrying components (for power delivery), monitoring, computing, communication and protection systems.
- Human interface power systems are not fully automated
- Complexity is increasing with more monitoring, control and communications
- Sources of failure:
  - physical components (power/current carrying),
  - failures in cyber network hard and soft,
  - human failures
- Contemporary power system reliability methods focused almost entirely on the failure of physical components

# Solution approaches in power system reliability evaluation

- Analytical methods: mostly used in single, multiarea and distribution system models.
- Monte Carlo simulation; mostly used in multi-area and composite system models.
- Intelligent search techniques: still in development stage for either increasing the efficiency of analytical or simulation or providing an alternative to Monte Carlo simulation.
- Hybrid: mixing for increased strength.
- An assumption running through the developed models and methods is that of independence of components and that cyber part is perfectly reliable.

# **Emerging Power Systems**

- Power systems of the future are emerging to be different.
- Two major factors contributing to this change:
  - Large penetration of renewable energy sources
  - Increasing complexity of cyber part.
- Installation of hardware for interactive relationship between the supplier and consumer will add to complexity and interdependency between the cyber and physical parts.
- Complexity and interdependency will introduce more sources of problems and make reliability analysis more challenging but also more essential.

# Introduction

#### **Cyber-Physical Security and Reliability**

Cyber Security: Studies deliberate cyber attack scenarios, consequences, and prevention or mitigation strategies.

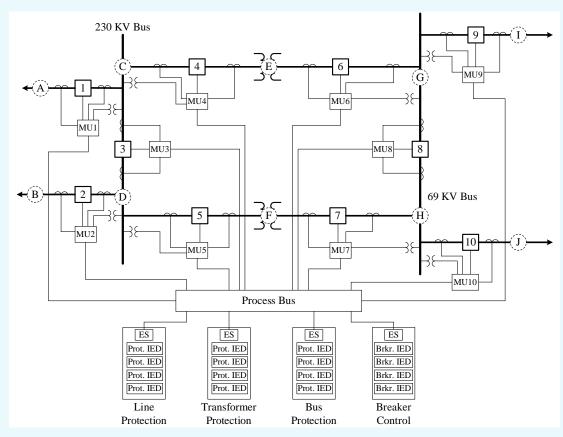
Cyber Reliability: Studies intrinsic failure modes of cyber related components and their impact on power system reliability.

Ultimately both impact the reliability of power supply but the two may require different modeling and methodology.

# **Cyber- Physical Interaction**

- The concepts and approaches will be explained using an example of a substation.
- The problems, however, extend across the entire grid.

#### **Digital Substation as a Cyber-Physical System**



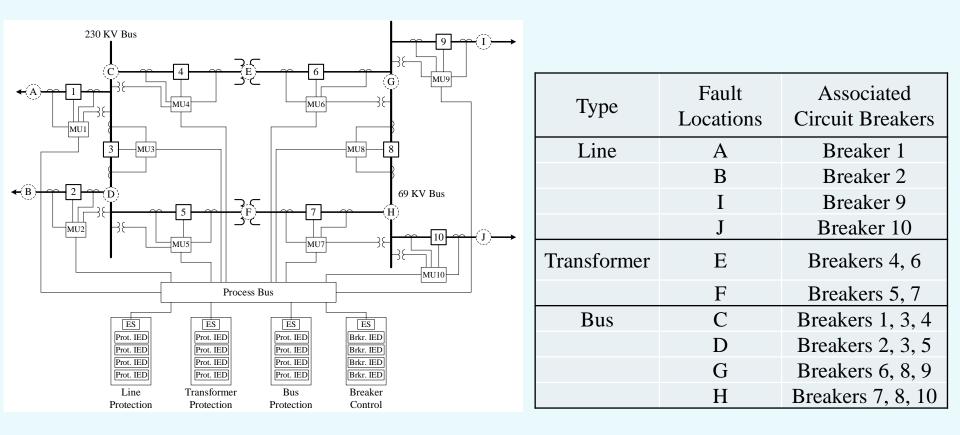
An IEC 61850 based protection system for a 230-69 kV substation

Physical Components (Power-Carrying Components): Transmission Lines Power Transformers **Circuit Breakers** Cyber Components: CTs/PTs **Merging Units** Process Bus

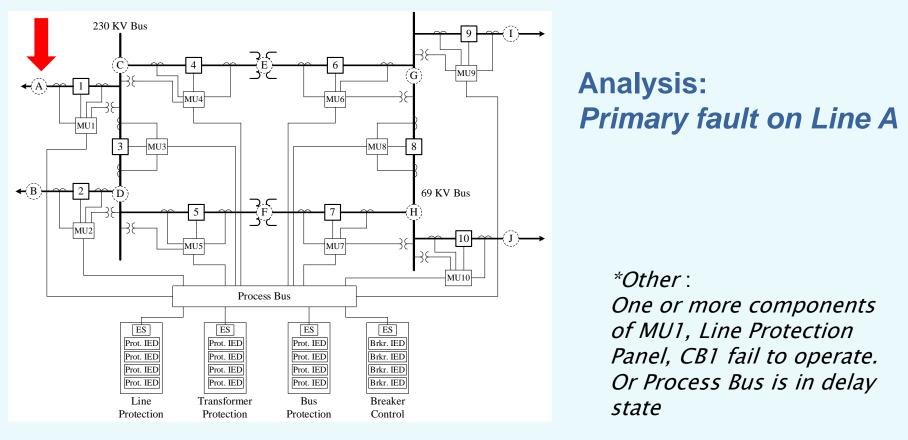
Ethernet Switches

**Protection IEDs** 

#### **Protection Zone Division**



### **How of Cyber-Physical Interdependency**



Failure Modes	Physical Components Affected	Probability
Protection all good	Only Line A	0.996957511
Process bus failed	Entire Substation	0.000009132
Other*	Line A and Bus C	0.003033357

### **Cyber-Physical Interdependency**

#### Analysis: Primary fault on Line B

Physical Components Affected	Probability
Only Line B	0.996957511
Entire Substation	0.000009132
Line B and Bus D	0.003033357

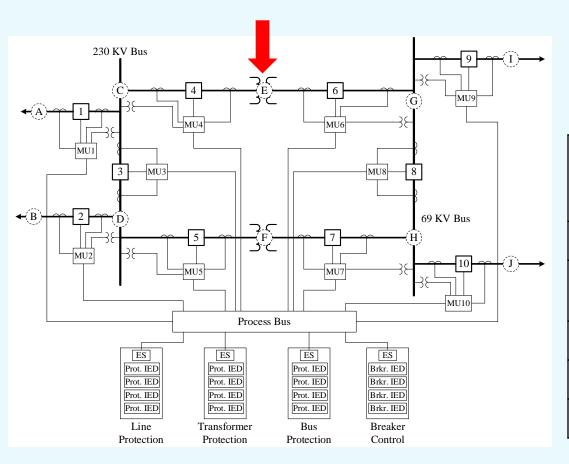
#### Analysis: Primary fault on Line I

Physical Components Affected	Probability
Only Line I	0.996957511
Entire Substation	0.000009132
Line I and Bus G	0.003033357

#### Analysis: Primary fault on Line J

Physical Components Affected	Probability
Only Line J	0.996957511
Entire Substation	0.000009132
Line J and Bus H	0.003033357

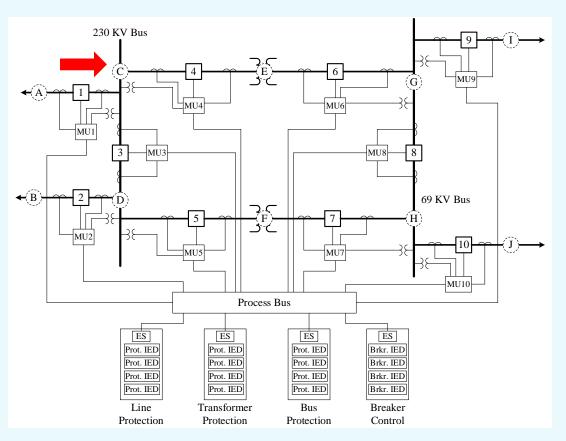
### **Cyber-Physical Interdependency**



Analysis: *Primary fault on Transformer E* 

Physical Components Affected	Probability
Only E	0.996942336
Entire Substation	0.000009132
E and C	0.000015174
E and G	0.000015174
E, C, and G	0.003018182

### **Cyber-Physical Interdependency**



Analysis: *Primary fault on Bus C* 

Physical Components Affected	Probability
Only C	0.996927163
Entire Substation	0.000009132
A and C	0.000015174
C and D	0.000015174
C and E	0.000015174
A, C, and D	2.31*10 <sup>-10</sup>
A, C, and E	2.31*10 <sup>-10</sup>
C, D, and E	2.31*10 <sup>-10</sup>
A, C, D, and E	0.003018182

#### **Representing interdependency for Reliability Analysis**

#### Cyber-Physical Interface Matrix (CPIM)

Line A	0.9969575	0.0000091	0.0030334	0	
Line B	0.9969575	0.0000091	0.0030334	0	
Line I	0.9969575	0.0000091	0.0030334	0	
Bus H	0.9969272	0.0000091	0.0000152	0.0000152	

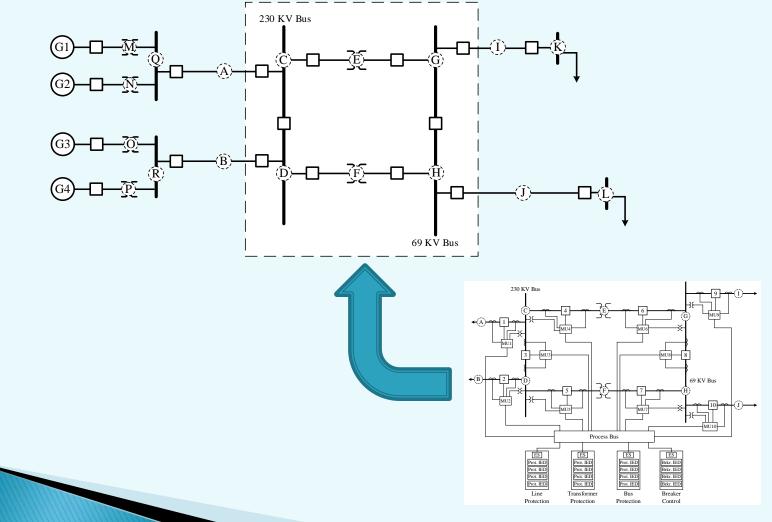
#### Consequent Events Matrix (CEM)

Line A	Event-1	Event-2	Event-3	Event-4	
Line B					
Line I					
Bus H					

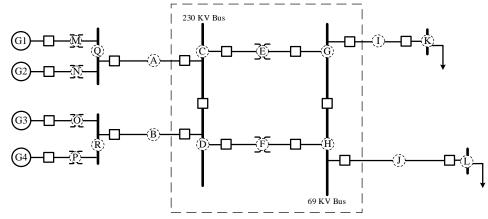
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### **System-wide Reliability Evaluation**

Composite system reliability evaluation with the use of cyber-physical interface matrix



Composite system reliability evaluation with the use of cyber-physical interface matrix



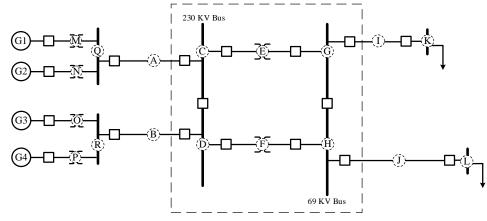
Step 1: Set the initial state of all components as UP and set the simulation time t = 0.

Step 2: For each individual component, draw a random decimal number  $z_i$  between 0 and 1 to compute the time to the next event.

$$T_i = -\frac{\ln(z_i)}{\rho_i}$$

Depending on whether the  $i^{th}$  component is UP or DOWN,  $\lambda_i$  or  $\mu_i$  is used in place of  $\rho_i$ 

Composite system reliability evaluation with the use of cyber-physical interface matrix



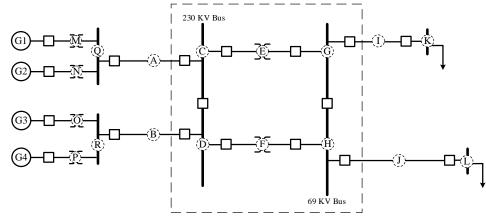
Step 3: Find the minimum time, change the state of the corresponding component, and update the total time.

 $T_q = \min\{T_i\}, 1 \le i \le N$ 

The next transition takes place by change of state of the  $q^{th}$  component. The total simulation time *t* is increased by  $T_{q}$ .

$$t = t + T_q$$

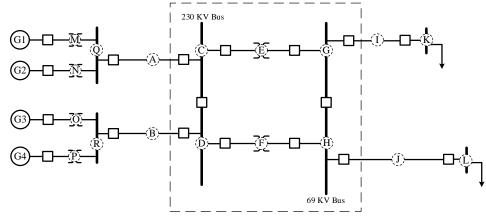
Composite system reliability evaluation with the use of cyber-physical interface matrix



Step 4: Change the  $q^{th}$  component's state accordingly. For each component *i* 

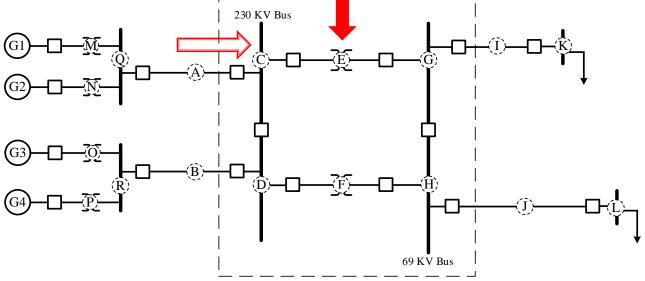
$$T_i = T_i - T_q$$

Composite system reliability evaluation with the use of cyber-physical interface matrix



Step 5: If the state of the *q*<sup>th</sup> component transits from UP to DOWN, which means a primary fault occurs on this component, then the cyber-physical interface matrix is used to determine if there are some subsequent failures causing more components out of service due to the cyber part's malfunction.

Composite system reliability evaluation with the use of cyber-physical interface matrix



Draw another random decimal number y (0 <  $y \le 1$ )

Line A	0.9969575	0.0000091	0.0030334	0	
Transformer E	0.9969423	0.0000091	0.0000152	0.0000152	
Bus H	9.9969272	0.0000091	0.0000152	0.0000152	

How to determine the next transition time of Transformer E and Bus C?

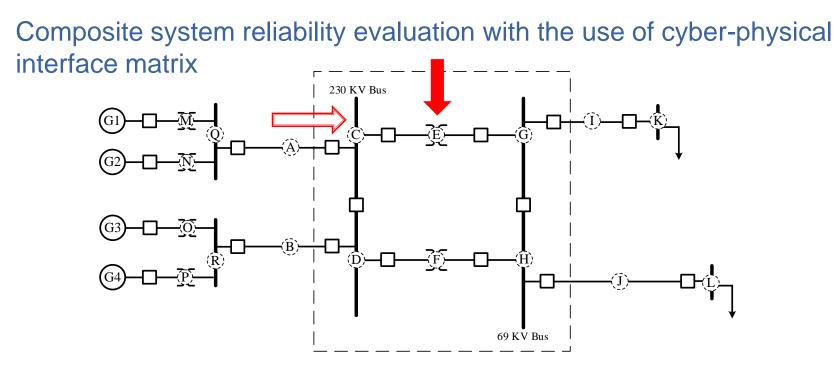
 $ln(z_i)$ 

 $\rho_i$ 

For Transformer E, use  $\mu_i$  in place of  $\rho_i$ 

For Bus C, use  $\mu_{i,exp}$  in place of  $\rho_i$ 

 $\mu_{i,exp}$  is an expedited repair rate, called switching rate

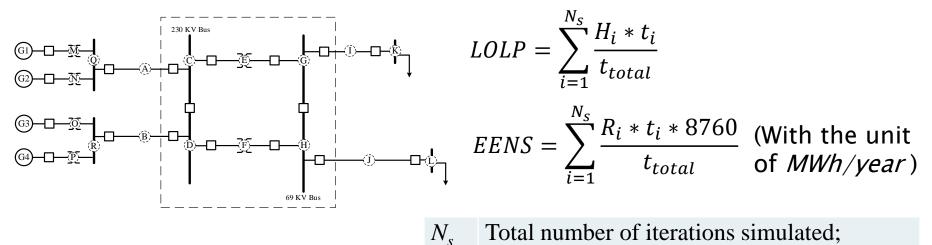


Step 6: Perform a network power flow analysis to assess system operation states. Update system-wide reliability indices.

Repeat steps 3–6 until convergence is achieved.

Composite system reliability evaluation with the use of cyber-physical interface matrix

When the simulation finishes, system-wide reliability indices can be obtained.



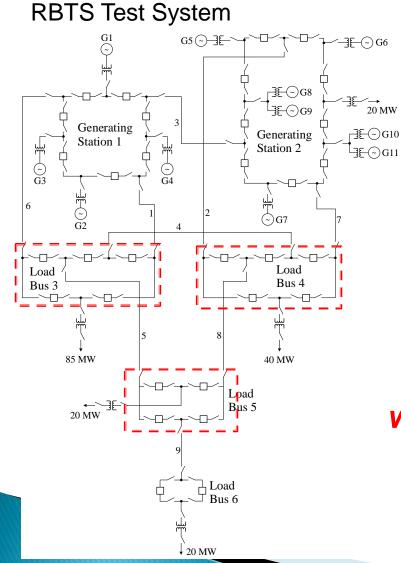
 $H_i$ 

LOLE = LOLP \* 8760 (With the unit of hours/year)

iteration; otherwise it equals 0; $t_i$ Simulated time in the  $i^{\text{th}}$  iteration, with the<br/>unit of year; $t_{total}$ Total simulated time, with the unit of year. $R_i$ Load curtailment during the  $i^{\text{th}}$  iteration,<br/>with the unit of MW;

Equals 1 if load curtailment occurs in the  $i^{th}$ 

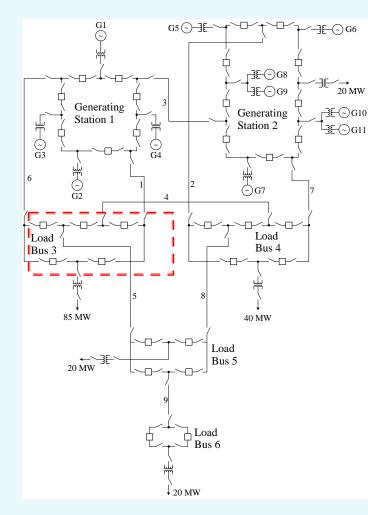
# Illustrating the overall methodology on a standard test system



#### System Configuration

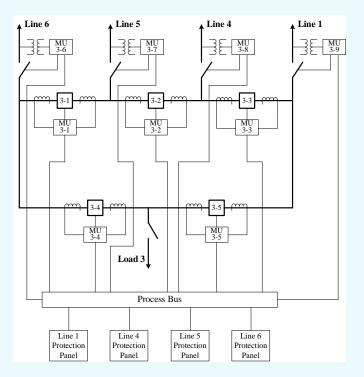
The size of this system is small to permit reasonable time for extension of cyber part and development of interface matrices. But the configuration of this system is sufficiently detailed to reflect the actual features of a practical system

# Buses 3–5 are extended with cyber configurations

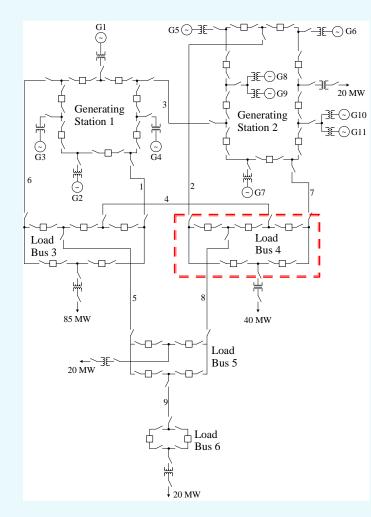


Physical part of the RBTS

Extend bus 3 of the RBTS Test System with substation protection configurations.

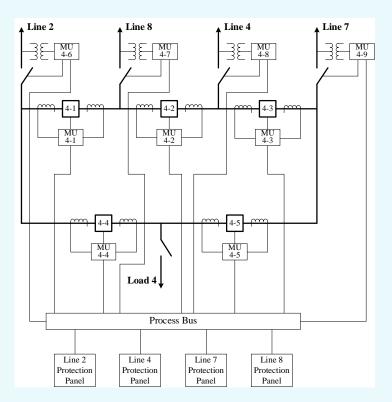


Extension with cyber part in Bus 3

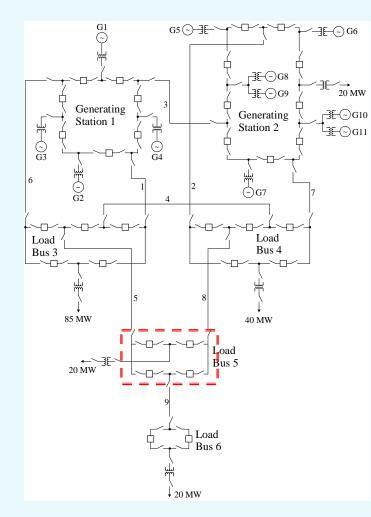


#### Physical part of the RBTS

Extend bus 4 of the RBTS with substation protection configurations.

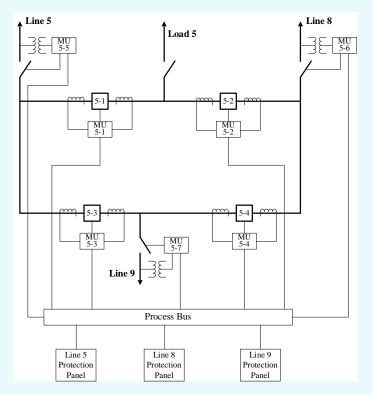


Extension with cyber part in Bus 4

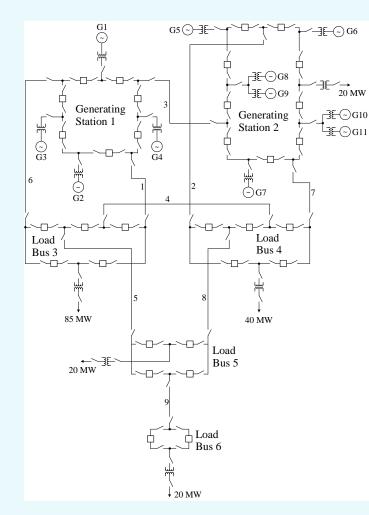


Physical part of the RBTS

Extend bus 5 of the RBTS with substation protection configurations.



Extension with cyber part in Bus 5



#### Physical part of the RBTS

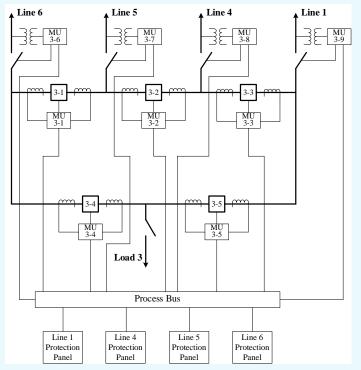
#### **Generation Variation**

Unit	Bu	Rating	Failure Rate	MRT (hours)
No.	s	(MW)	(/year)	
1	1	40	6.0	45
2	1	40	6.0	45
3	1	10	4.0	45
4	1	20	5.0	45
5	2	5	2.0	45
6	2	5	2.0	45
7	2	40	3.0	60
8	2	20	2.4	55
9	2	20	2.4	55
10	2	20	2.4	55
11	2	20	2.4	55

#### Load Variation

The hourly load profile is created based on the information in Tables 1, 2, and 3 of the IEEE Reliability Test System<sup>\*</sup>.

\*IEEE Committee Report, "IEEE reliability test system," *IEEE Trans. Power App. and Syst.*, vol. PAS-98, no. 6, pp. 2047–2054, Nov./Dec. 1979.



p <sub>1,1</sub>	$p_{1,2}$		$p_{1,n}$ ]
$p_{2,1}$	$p_{2,2}$	•••	$p_{2,n}$
	•	•.	:
$p_{m,1}$	$p_{m,2}$	•••	$p_{m,n}$

Analyze the cyber failure modes and consequent events and obtain the Cyber-Physical Interface Matrices (CPIM) for Buses 3-5.

#### Results: The CPIM and CEM of Bus 3

#### The Cyber-Physical Interface Matrix (CPIM) of Bus 3

Fault	Probabilities						
Location							
Line 1	0.996899850569	0.000009132337	0.000027312491	0.000027312491	0.003036392112		
Line 4	0.996899850569	0.000009132337	0.000027312491	0.000027312491	0.003036392112		
Line 5	0.996899850569	0.000009132337	0.000027312491	0.000027312491	0.003036392112		
Line 6	0.996899850569	0.000009132337	0.000027312491	0.000027312491	0.003036392112		

#### The Consequent Event Matrix (CEM) of Bus 3

Fault	Events				
Location	Events				
Line 1	10000000000	100111000000	10010000000	10000000100	100100000100
Line 4	000100000000	100111000000	000110000000	10010000000	100110000000
Line 5	000010000000	100111000000	000011000000	000110000000	000111000000
Line 6	000001000000	100111000000	000001000100	000011000000	000011000100

#### Results: The CPIM and CEM of Bus 4

#### The Cyber-Physical Interface Matrix (CPIM) of Bus 4

Fault	Probabilities						
Location	Probabilities						
Line 2	0.996899850569	0.996899850569 0.000009132337 0.000027312491 0.000027312491 0.003036392112					
Line 4	0.996899850569	0.000009132337	0.000027312491	0.000027312491	0.003036392112		
Line 7	0.996899850569	0.000009132337	0.000027312491	0.000027312491	0.003036392112		
Line 8	0.996899850569	0.000009132337	0.000027312491	0.000027312491	0.003036392112		

#### The Consequent Event Matrix (CEM) of Bus 4

Fault	Events				
Location	Events				
Line 2	01000000000	010100110000	01000000010	010000010000	010000010010
Line 4	00010000000	010100110000	000100010000	000100100000	000100110000
Line 7	000000100000	010100110000	000100100000	000000100010	000100100010
Line 8	00000010000	010100110000	010000010000	000100010000	010100010000

#### Results: The CPIM and CEM of Bus 5

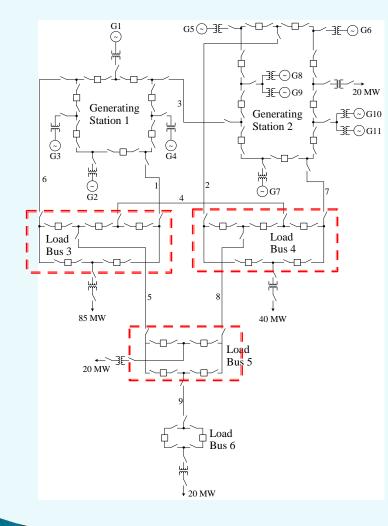
#### The Cyber-Physical Interface Matrix (CPIM) of Bus 5

Fault	Probabilities				
Location	Flobabilities				
Line 5	0.996899850569	0.000009132337	0.000027312491	0.000027312491	0.003036392112
Line 8	0.996899850569	0.000009132337	0.000027312491	0.000027312491	0.003036392112
Line 9	0.996899850569	0.000009132337	0.000027312491	0.000027312491	0.003036392112

#### The Consequent Event Matrix (CEM) of Bus 5

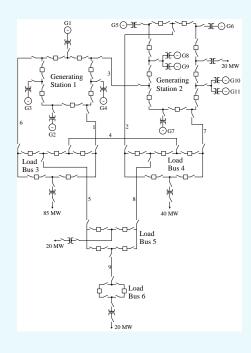
Fault			Evente		
Location	Events				
Line 5	000010000000	000010011000	000010001000	000010000001	000010001001
Line 8	00000010000	000010011000	00000010001	000000011000	00000011001
Line 9	00000001000	000010011000	00000011000	000010001000	000010011000

### Stage 2: Composite System Level Analysis



Utilize the results of the interface matrices, perform a Monte-Carlo simulation for the composite system, and obtain numerical results of system-wide reliability indices.

### Stage 2: Composite System Level Analysis



Objective:  $y = Min \sum_{i=1}^{N_b} C_i$ 

subject to:

$$\hat{B}\theta + G + C = L$$

$$G \leq G^{max}$$

$$C \leq L$$

$$DA\theta \leq F^{max}$$

$$-DA\theta \leq F^{max}$$

$$G, C \geq 0$$

$$\theta_1 = 0$$

$$\theta_2 \quad N_k \text{ unrestricted}$$

Variables:  $\theta$ , G, and C

Total number of variables:  $3N_h$ 

 $N_{b}$ C $N_h \times 1$  vector of bus load curtailments  $C_i$ Load curtailment at bus *i* Â  $N_h \times N_h$  augmented node susceptance matrix

Number of buses

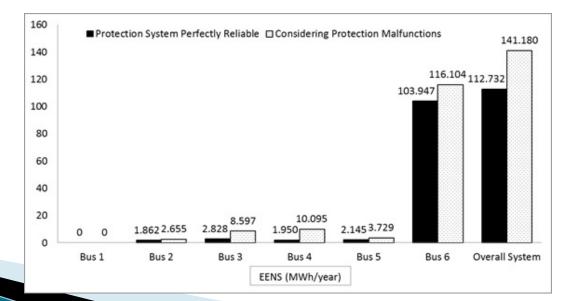
- $N_b \times 1$  vector of bus actual G generating power
- $G^{max}$  $N_h \times 1$  vector of bus maximum generating availability
- $N_h \times 1$  vector of bus loads L
- $N_t \times N_t$  diagonal matrix of D transmission line susceptances, with  $N_t$  the number of transmission lines
- A  $N_t \times N_b$  line-bus incidence matrix
- $N_h \times 1$  vector of bus voltage  $\theta$ angles
- **F**max  $N_t \times 1$  vector of transmission line power flow capacities

### Stage 2: Composite System Level Analysis

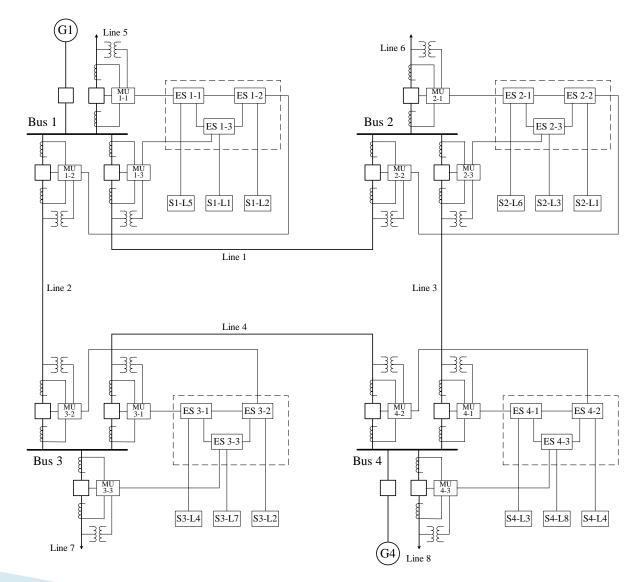
#### **Brief Results**

#### Impact on Expected Energy Not Served (EENS)

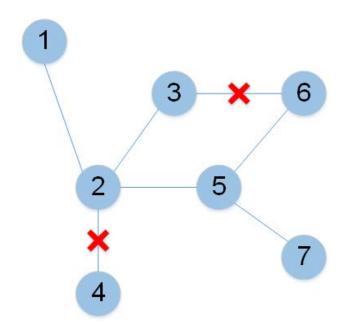
	EENS (MWh/year)		
	If protection systems are perfectly reliable	Considering protection malfunctions	
Bus 1	0	0	N/A
Bus 2	1.862	2.655	42.59%
Bus 3	2.828	8.597	204.00%
Bus 4	1.950	10.095	417.69%
Bus 5	2.145	3.729	73.85%
Bus 6	103.947	116.104	11.70%
Overall System	112.732	141.180	25.24%



# **Modeling Cyber Link Failures**



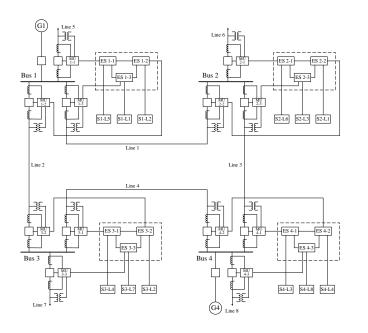
# **Modeling Cyber Link Failures**

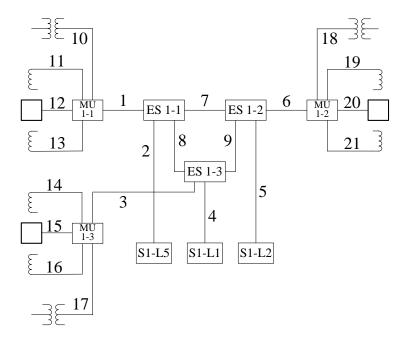


Two types of cyber link failures:

- (a) A link is unavailable due to packet delay resulting from traffic congestion or queue failure;
- (b) A link is physically damaged.

Failure type (b) is relatively rare and thus only failure type (a) is considered in this research





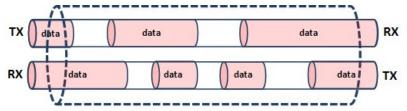
### Reliability Data for Components

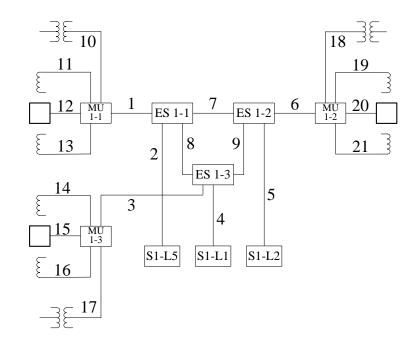
Component	Failure Rate (/year)	Mean Repair Time (h)
Circuit Breaker	0.01	8
Merging Unit	0.02	8
Ethernet Switch	0.01	8
Line Protection Panel	0.02	8

#### Cyber Component Names and Meanings

Component Name	Meaning
MU 1-1	Merging Unit 1 at Substation 1
MU 1-2	Merging Unit 2 at Substation 1
MU 1-3	Merging Unit 3 at Substation 1
ES 1-1	Ethernet Switch 1 at Substation 1
ES 1-2	Ethernet Switch 2 at Substation 1
ES 1-3	Ethernet Switch 3 at Substation 1
S1-L5	Line 5 Protection Panel at Substation 1
S1-L1	Line 1 Protection Panel at Substation 1
S1-L2	Line 2 Protection Panel at Substation 1

Cyber Component Names and Meanings			
Meaning			
Merging Unit 1 at Substation 1			
Merging Unit 2 at Substation 1			
Merging Unit 3 at Substation 1			
Ethernet Switch 1 at Substation 1			
Ethernet Switch 2 at Substation 1			
Ethernet Switch 3 at Substation 1			
Line 5 Protection Panel at Substation 1			
Line 1 Protection Panel at Substation 1			
Line 2 Protection Panel at Substation 1			





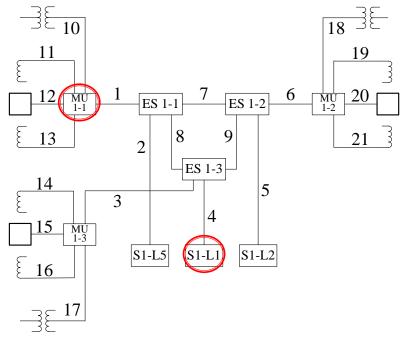
For the link *i*, the time it takes for a packet to travel in the forward direction is a random variable denoted by  $t_{i,1}$ For the reverse direction, the random time is denoted by  $t_{i,2}$ 

### For example:

Consider Link 7, the time it takes for a packet to travel from ES 1-1 to ES 1-2 is denoted by  $t_{7,1}$ 

From ES 1-2 to ES 1-1, the time is denoted by  $t_{7,2}$ 

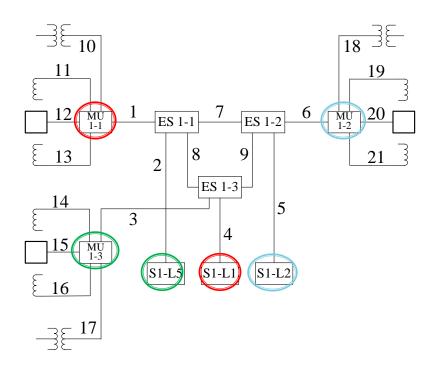
Cyber Component Names and Meanings			
Component Name	Meaning		
MU 1-1	Merging Unit 1 at Substation 1		
MU 1-2	Merging Unit 2 at Substation 1		
MU 1-3	Merging Unit 3 at Substation 1		
ES 1-1	Ethernet Switch 1 at Substation 1		
ES 1-2	Ethernet Switch 2 at Substation 1		
ES 1-3	Ethernet Switch 3 at Substation 1		
S1-L5	Line 5 Protection Panel at Substation 1		
S1-L1	Line 1 Protection Panel at Substation 1		
S1-L2	Line 2 Protection Panel at Substation 1		



Consider the communication from MU 1-1 to S1-L1. There are two possible paths: 1-8-4 and 1-7-9-4.

$$p_{fail} = \Pr[(t_{1.1} + t_{8.1} + t_{4.1} > T_{tsd}) and (t_{1.1} + t_{7.1} + t_{9.1} + t_{4.1} > T_{tsd})]$$

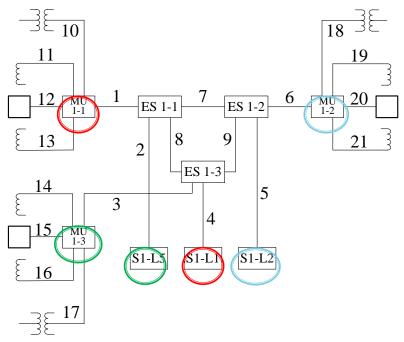
where  $T_{tsd}$  is a predefined threshold delay value for the two paths.



From MU 1-1 to S1-L1

 $\begin{aligned} p_{fail} &= \Pr[(t_{1.1} + t_{8.1} + t_{4.1} > T_{tsd}) \ and \ (t_{1.1} + t_{7.1} \\ &+ t_{9.1} + t_{4.1} > T_{tsd})] \end{aligned}$ 

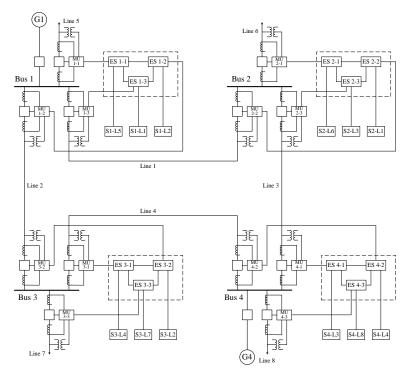
Similarly, with any two components specified as the two ends of a communication path, the path failure probability can be computed from the cyber link level parameters



The detailed procedures are based on queueing theory and are beyond the scope of this research. These probabilities can be assumed directly at the path level.

From	То	Forward Path Failure Probability	Reverse Path Failure Probability
MU 1-1	S1-L5	0.002	0.002
MU 1-1	S1-L1	0.001	0.001
MU 1-1	S1-L2	0.001	0.001
MU 1-2	S1-L5	0.001	0.001
MU 1-2	S1-L1	0.001	0.001
MU 1-2	S1-L2	0.002	0.002
MU 1-3	S1-L5	0.001	0.001
MU 1-3	S1-L1	0.002	0.002
MU 1-3	S1-L2	0.001	0.001

Results



The Cyber-Physical Interface Matrix

Primary				
Fault	Probabilities of Consequent Events			
Location				
Line 1	0.9919152	0.0040342	0.0040342	0.0000164
Line 2	0.9919152	0.0040342	0.0040342	0.0000164
Line 3	0.9919152	0.0040342	0.0040342	0.0000164
Line 4	0.9919152	0.0040342	0.0040342	0.0000164
Line 5	0.9959494	0.0040506	0	0
Line 6	0.9959494	0.0040506	0	0
Line 7	0.9959494	0.0040506	0	0
Line 8	0.9959494	0.0040506	0	0

#### The Consequent Event Matrix

Primary				
Fault	Consequent Events			
Location				
Line 1	1000000	11001000	10100100	11101100
Line 2	01000000	11001000	01010010	11011010
Line 3	00100000	10100100	00110001	10110101
Line 4	00010000	01010010	00110001	01110011
Line 5	00001000	11001000	00000000	00000000
Line 6	00000100	10100100	00000000	00000000
Line 7	00000010	01010010	00000000	00000000
Line 8	00000001	00110001	00000000	00000000

## **Comments on Scalability**

### Stage 1: Substation Level Analysis

Analysis at this stage can be performed locally at each substation and the computations can be performed **offline**.

### Stage 2: Composite System Level Analysis

The results of CPIMs and CEMs can be directly utilized. Monte-Carlo simulation performed in this stage is generic and applicable for large power systems.

The CPIM decouples the 2 stages of analysis, making the overall analysis more tractable.

### **Further work**

- Cyber-Physical Interactions Modeling
  - This is only starting point
  - More detailed models need to be developed.
  - We need to consider inter-substation interactions
  - Consider the interaction of physical on the cyber as well
  - More automated analysis at the substation level.

### **Further Work**

- Computational Methods Development
  - Generally non-sequential Monte Carlo Simulation is preferred as a more efficient method of for reliability evaluation.
  - Several variance reduction techniques like importance sampling have been developed to make it even faster, especially those incorporating the concept of cross-entropy.
  - The efficiency of non-sequential MCS is based on the assumption of independence between the components, although limited dependence can be accommodated.

### **Further Work**

- Because of interdependence introduced by cyber part it becomes difficult to use nonsequential MC and the associated variance reduction techniques. So we have used sequential MCS.
- We have also proposed a non-sequential MCS technique to solve this problem but more work is needed in this direction.

## **Test System**

- IEEE RTS Reliability Test System has served as a resource for the researchers and developers to test their algorithms and compare their results with others.
- Additional information about distribution has since been added.
- This test system does not have information on the related cyber part.
- A taskforce under the Reliability, Risk and Probability Applications Subcommittee (RRPA) is investigating adding configurations and data on the cyber part.

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## Acknowledgements

This presentation is based on the work of my students Yan Zhang and Hangtian Lei.

The work reported here was supported in part by PSERC Project T-53.

### **Questions?**

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